

0.1 The Eigenvalue Problem

$$\left. \begin{aligned} \frac{d^2 \Psi(x^*)}{dx^{*2}} - l^2 \Psi(x^*) &= 0, \quad \Psi(0) = 0, \Sigma(1) = 0, \\ \frac{d^2 \Sigma(x^*)}{dx^{*2}} - l^2 \Sigma(x^*) &= 0, \quad \Psi(S_0^*) = \Sigma(S_0^*) + \Phi N_0, \end{aligned} \right\} \quad (1)$$

The solutions of (1) for the pressure eigenfunctions subject to the pressure continuity condition (1) are

$$\left. \begin{aligned} \Psi(x^*) &= 2 C_3 \sinh(l x^*), \\ \Sigma(x^*) &= 2 C_4 \frac{\sinh(l(x^* - 1))}{\cosh(l) - \sinh(l)}, \end{aligned} \right\} \quad (2)$$

where the constant of integration are

$$\begin{aligned} C_3 &= \frac{1}{2} \frac{\Phi}{l} \left[\frac{\left\{ \varphi \sigma (1 - R_1) + \coth(l(S_0^* - 1)) l N_0 \right\}}{\sinh(l S_0^*) \left\{ R \coth(l(S_0^* - 1)) - \coth(l S_0^*) \right\}} \right], \\ C_4 &= \frac{1}{2} \frac{\Phi}{l} \left[\frac{\left\{ \varphi \sigma (1 - R_1) + \coth(l S_0^*) l N_0 \right\} \left\{ \cosh(l) - \sinh(l) \right\}}{\sinh(l(S_0^* - 1)) \left\{ R \coth(l(S_0^* - 1)) - \coth(l S_0^*) \right\}} \right]. \end{aligned}$$

where

$$\begin{aligned} N_0 &= F_1(S_0^*) \frac{C}{k} \frac{Pec_i}{R} \left\{ (R - 1) + \frac{k R R_3 (1 - R_1)}{C Pec_i} \right\}. \\ F(S_0^*) &= \frac{\dot{m}_{liq,vap}}{\dot{m}_i} = F_1(S_0^*) [1 - R G_1 S_0^*], \quad F_1(S_0^*) = \frac{1}{R S_0^* + 1 - S_0^*}, \\ G_1 &= \frac{R_3 k (1 - R_1)}{C Pec_i}. \end{aligned} \quad (3)$$

The eigenvalue problem for the temperature distributions in the both phases,

$$\left. \begin{aligned} & \left(\frac{d^2}{dx^{*2}} - \omega_0 \frac{d}{dx^*} - E_1 \sigma - l^2 \right) \phi_{liq} + \frac{d\Theta_{liq}^0}{dx^*} \frac{d\Psi}{dx^*} = 0, \\ & \phi_{liq}(0) = 0, \quad \phi_{liq}(S_0^*) = -\Phi \left. \frac{d\Theta_{liq}^0}{dx^*} \right|_{x^*=S_0^*}, \\ & \left(\frac{d^2}{dx^{*2}} - \Omega_0 \frac{d}{dx^*} - \frac{E_2 k R_1}{C} \sigma - l^2 \right) \phi_{vap} + \frac{R k}{C} \frac{d\Theta_{vap}^0}{dx^*} \frac{d\Sigma}{dx^*} = 0, \\ & \phi_{vap}(1) = 0, \quad \phi_{vap}(S_0^*) = -\Phi \left. \frac{d\Theta_{vap}^0}{dx^*} \right|_{x^*=S_0^*}, \end{aligned} \right\} \quad (4)$$

where

$$\left. \begin{aligned} & \frac{d\Theta_{liq}^0}{dx^*} = N_1 \exp(\omega_0 x^*), \\ & \frac{d\Theta_{vap}^0}{dx^*} = N_2 \exp(\Omega_0 (x^* - 1)), \end{aligned} \right\} \quad (5)$$

with leads to

$$\left. \frac{d\Theta_{liq}^0}{dx^*} \right|_{x^*=S_0^*} = N_3, \quad \text{and} \quad \left. \frac{d\Theta_{vap}^0}{dx^*} \right|_{x^*=S_0^*} = N_4, \quad (6)$$

where

$$\left. \begin{aligned} & N_1 = \frac{\omega_0}{\exp(\omega_0 S_0^*) - 1}, \quad N_2 = \frac{\Omega_0}{\exp(\Omega_0 (S_0^* - 1)) - 1}, \\ & N_3 = N_1 \exp(\omega_0 S_0^*), \quad N_4 = N_2 \exp(\Omega_0 (S_0^* - 1)). \end{aligned} \right\} \quad (7)$$

and

$$\left. \begin{aligned} & \omega_0 = \frac{1}{k} Pec_i F(S_0^*) C, \\ & \Omega_0 = Pec_i F(S_0^*), \end{aligned} \right\} \quad (8)$$

The solution of (4) for the eigenfunction of the liquid temperature distribution is

$$\begin{aligned} \phi_{liq}(x^*) = & \frac{C_3 l N_1}{f_1 f_4 f_5 f_6} \left\{ f_1 f_4 f_6 \exp(x^*(\omega_0 - 1)) + \left\{ 2 f_1 f_4 E_1 \sigma \cosh\left(\frac{\gamma_3 x^*}{2}\right) \right. \right. \\ & \left. \left. - \left[2 f_1 f_2 E_1 \sigma + f_6 f_7 - f_3 f_5 \right] \sinh\left(\frac{\gamma_3 x^*}{2}\right) \right\} \exp\left(\frac{x^* \omega_0}{2}\right) \right\} \end{aligned}$$

$$-f_1 f_4 f_5 \exp(x^*(\omega_0 + 1)) \Big\} - \frac{\Phi N_3}{f_1 f_4} \exp\left(\frac{x^* \omega_0}{2}\right) \sinh\left(\frac{\gamma_3 x^*}{2}\right), \quad (9)$$

where

$$\begin{aligned} \gamma_3 &= \sqrt{\omega_0^2 + 4 E_1 \sigma + 4 l^2}, \quad f_1 = \exp\left(\frac{\omega_0 S_0^*}{2}\right), \quad f_2 = \cosh\left(\frac{\gamma_3 S_0^*}{2}\right), \\ f_3 &= \exp((\omega_0 + l) S_0^*), \quad f_4 = \sinh\left(\frac{\gamma_3 S_0^*}{2}\right), \quad f_5 = (\omega_0 l + E_1 \sigma), \\ f_6 &= (\omega_0 l - E_1 \sigma), \quad f_7 = \exp(S_0^* (\omega_0 - l)). \end{aligned}$$

The solution of (4) for the vapour temperature distribution is

$$\begin{aligned} \phi_{vap}(x^*) &= \frac{C_4 N_2}{f_{19}} \left\{ f_{20} \exp((\Omega_0 - l)x^* - \Omega_0 + 2l) + f_{21} \exp\left(\frac{\Omega_0 x^*}{2}\right) \sinh\left(\frac{\gamma_4 x^*}{2C}\right) \right. \\ &\quad \left. - f_{22} \left\{ f_{23} \exp\left(\frac{\Omega_0 x^*}{2}\right) \cosh\left(\frac{\gamma_4 x^*}{2C}\right) + f_{13} \exp((\Omega_0 + l)x^* - \Omega_0) \right\} \right\} \\ &\quad - \Phi N_2 f_{24} \exp\left(\frac{x^* \Omega_0}{2}\right) \sinh\left(\frac{\gamma_4 x^*}{2C}\right), \quad (10) \end{aligned}$$

where

$$\begin{aligned} \gamma_4 &= \sqrt{((\Omega_0^2 + 4 l^2) C^2 + 4 E_1 \sigma C k R_1)}, \quad f_8 = (C \Omega_0 l - k R_1 E_1 \sigma), \\ f_9 &= \exp\left(\frac{\Omega_0 S_0^*}{2}\right), \quad f_{10} = \sinh\left(\frac{\gamma_4 S_0^*}{2C}\right), \quad f_{11} = \exp(-\Omega_0), \\ f_{12} &= \exp(-\Omega_0 + 2l), \quad f_{13} = (C \Omega_0 l + k R_1 E_1 \sigma), \quad f_{14} = \cosh\left(\frac{\gamma_4 S_0^*}{2C}\right), \\ f_{15} &= \exp(\Omega_0(S_0^* - l)), \quad f_{16} = \exp((\Omega_0 + l) S_0^* - \Omega_0), \\ f_{17} &= \exp(\Omega_0(S_0^* - 1) - l(S_0^* - 2)), \quad f_{18} = E_1^2 \sigma^2 + C^2 \Omega_0^2 l^2 - k^2 R_1^2, \\ f_{19} &= f_9 f_{10} f_{18}, \quad f_{20} = f_{22} f_8, \quad f_{22} = R k l f_9 f_{10}, \quad f_{24} = \frac{f_8 f_{13} f_{15}}{f_{19}}, \end{aligned}$$

$$f_{21} = R k l \left\{ f_9 f_{12} f_{14} (C \Omega_0 l - R_1 E_1 \sigma k) - f_8 f_{17} - f_9 f_{11} f_{13} f_{14} + f_{13} f_{16} \right\},$$

$$f_{23} = \left\{ f_{12} (C \Omega_0 l - R_1 E_1 \sigma k) - f_{11} f_{13} \right\}.$$

0.2 Dispersion Analysis

An equation which represent the relationship between the decay rate σ and the wave number l is known as dispersion equation and can be obtained by using the energy jump across the liquid-vapour interface.

$$\varphi \sigma H_{liq} \Phi = \left\{ \Phi \frac{d^2 \Theta_{liq}^0}{dx^{*2}} + \frac{d\phi_{liq}}{dx^*} \right\} + \frac{\Theta_0}{k} \left\{ \Phi \frac{d^2 \Theta_{vap}^0}{dx^{*2}} + \frac{d\phi_{vap}}{dx^*} \right\} - H_{liq} \frac{d\Psi_1}{dx^*}. \quad (11)$$

From the basic state we know that

$$\left. \begin{aligned} \frac{d^2 \Theta_{liq}^0}{dx^{*2}} \Big|_{x^*=S_0^*} &= N_3 \omega_0, \\ \frac{d^2 \Theta_{vap}^0}{dx^{*2}} \Big|_{x^*=S_0^*} &= N_4 \Omega_0. \end{aligned} \right\} \quad (12)$$

Substituting (12) into (11) yields

$$\varphi \sigma H_{liq} \Phi = \left\{ \frac{d\phi_{liq}}{dx^*} + \Phi N_3 \omega_0 \right\} + \frac{\Theta_0}{k} \left\{ \frac{d\phi_{vap}}{dx^*} + \Phi N_4 \Omega_0 \right\} - H_{liq} \frac{d\Psi_1}{dx^*}. \quad (13)$$

The complete solution for $\sigma(l)$ has been obtained by substituting (2), (9) and (10) into (13) which is solved numerically using Maple.

I want to solve (13) for $\sigma(l)$ considering two cases

1. taking limit of (13) when $\sigma \rightarrow 0$ and $l \rightarrow 0$ to find R_3 . using this R_3 and will plot $\sigma(l)$ to check the stability
2. taking limit of (13) when $\sigma \rightarrow 0$ and $l \rightarrow \infty$ to find R_3 . using this R_3 and will plot $\sigma(l)$ to check the stability

If you have time then plz help me to find a way to get the solution in more readable form.

Note

The value of S_0^* show be obtained first from the following equation

$$\frac{\Theta_0}{C} = \{\exp [Pec_i F(S_0^*) (1 - S_0^*)] - 1\} \left\{ H_{liq} + \frac{1}{1 - \exp \left[-\frac{C F(S_0^*) Pec_i S_0^*}{k} \right]} \right\} \quad (14)$$

The values of the parameters are parvals:= $\varphi = 0.38$, $R_1 = 0.0009$, $R_2 = 8.75$, $E_1 = 1$, $E_2 = 1$,

$$C = 1.96, \quad k = 4, \quad H_{liq} = 7, \quad Pec_i = -120, \quad \Phi = 1, \quad \Theta_0 = 1.9, R = 20$$